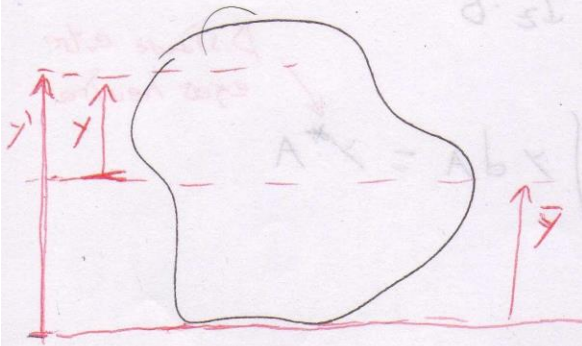


\* Cálculo de propiedades de Área ( $I_z, Q$ )

↳ 2º momento de área ( $\bar{I}_z$ )



$$\bar{y} \text{ (Eje neutro)} = \frac{\int y' dA}{A}$$

$$\bar{I}_z = \int y'^2 dA = \int (y' - \bar{y})^2 dA$$

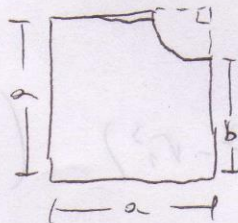
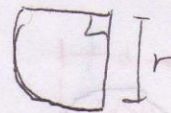
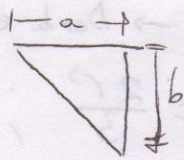
• Si hay varias fig. geométricas

$$\bar{y}_T = \frac{\sum \bar{y}_i \cdot A_i}{\sum A_i}$$

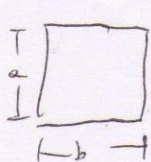
• Traslado de eje de rotación (Teorema de los ejes paralelos)

$$\bar{I}_z = I_z + d^2 A$$

\* Encontrar eje neutro y  $I_z$  de:



\* Secciones conocidas:



$$I_z = \frac{ba^3}{12}$$



$$I_z = \frac{\pi d^4}{64}$$

- Cálculo de deflexión por integración:

$$\frac{d^4 y}{dx^4} = -\frac{w(x)}{EI} \quad \leftarrow \text{Fza distribuida}$$


\* Modelación de Fzas mediante función escalón ( $v(x-x_0)$ ) para Fzas distribuidas, y delta de Dirac ( $\delta(x-x_0)$ ) para Fzas puntuales

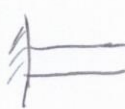
\* Lo que ocurre en los extremos de la viga se reemplaza por condiciones de borde (Se necesitan 4 cond. de borde)


\* Las cond. de borde son condiciones en la deflexión en los extremos, el ángulo de deflexión ( $\frac{dy}{dx}$ ), el momento ( $\frac{d^2 y}{dx^2}$ ) o de Fza de corte ( $\frac{d^3 y}{dx^3}$ )

$$\hookrightarrow \boxed{M = EI \frac{d^2 y}{dx^2}} \quad \wedge \quad \boxed{V = -EI \frac{d^3 y}{dx^3}}$$

\* Algunos bordes:

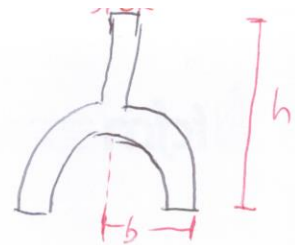
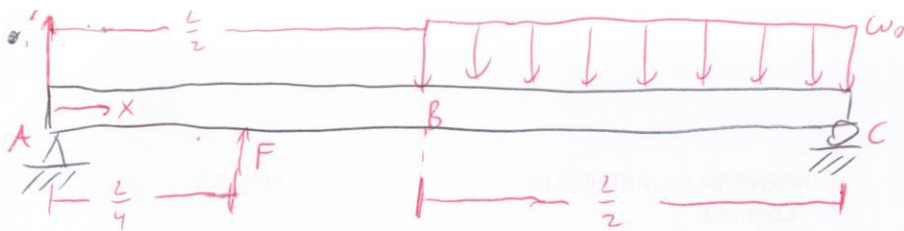
  $\Rightarrow$  No hay deflexión  $\rightarrow y(0) = 0$   
 No hay momento  $\rightarrow \frac{d^2 y}{dx^2} = 0$

  $\Rightarrow$  No hay deflexión  $\rightarrow y(0) = 0$   
 No hay ángulo  $\rightarrow \frac{dy}{dx}(0) = 0$

  $\Rightarrow$  No hay momento  $\rightarrow \frac{d^2 y}{dx^2}(0) = 0$

Balace de fzas  $\rightarrow V(0) = -F = -k y(0)$   
 $\therefore -EI \frac{d^3 y}{dx^3}(0) = -k y(0)$





(1): Semicírculo de radio  $b$  completo  
 (2): Semicírculo de radio  $(b-e)$

$$\bar{Y}_T = \frac{\sum A_i Y_i}{\sum A_i} = \frac{Y_1 \cdot A_1 - Y_2 \cdot A_2 + Y_3 \cdot A_3}{A_1 - A_2 + A_3}$$

$$\begin{aligned} * Y_1 &= \frac{4b}{3\pi} & * Y_2 &= \frac{4(b-e)}{3\pi} & * Y_3 &= \frac{(h-b)}{2} + b = \frac{b+h}{2} \\ A_1 &= \frac{\pi b^2}{2} & A_2 &= \frac{\pi(b-e)^2}{2} & A_3 &= e(h-b) \end{aligned}$$

Desde la base!

$$\therefore \bar{Y}_T = 0,07468 \text{ m} = 7,468 \text{ cm}$$

$$b) \bar{I}_T = (\bar{I}_1 - \bar{I}_2 + \bar{I}_3) \leftarrow \text{Cr a eje neutro de fig. completa } \bar{Y}_T$$

$$\begin{aligned} \rightarrow I_1 &= 0,1098 b^4 \Rightarrow \bar{I}_1 = I_1 + (Y_1 - \bar{Y}_T)^2 \cdot A_1 \\ &= 0,1098 b^4 + \left(\frac{4b}{3\pi} - \bar{Y}_T\right)^2 \cdot \frac{\pi b^2}{2} = 1643,56 \text{ cm}^4 \end{aligned}$$

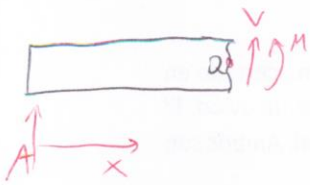
$$\begin{aligned} \rightarrow I_2 &= 0,1098 (b-e)^4 \Rightarrow \bar{I}_2 = I_2 + (Y_2 - \bar{Y}_T)^2 \cdot A_2 \\ &= 0,1098 (b-e)^4 + \left(\frac{4(b-e)}{3\pi} - \bar{Y}_T\right)^2 \cdot \frac{\pi (b-e)^2}{2} \\ &= 2413,88 \text{ cm}^4 \end{aligned}$$

$$\begin{aligned} \rightarrow I_3 &= \frac{e \cdot (h-b)^3}{12} \Rightarrow \bar{I}_3 = I_3 + (Y_3 - \bar{Y}_T)^2 \cdot A_3 \\ &= \frac{e(h-b)^3}{12} + \left(\frac{(h+b)}{2} - \bar{Y}_T\right)^2 \cdot e(h-b) = 283,28 \text{ cm}^4 \end{aligned}$$

$$\therefore \bar{I}_T = 4340,72 \text{ cm}^4 = 4,341 \cdot 10^{-5} \text{ m}^4$$

c) Momento interno  $M(x)$ :

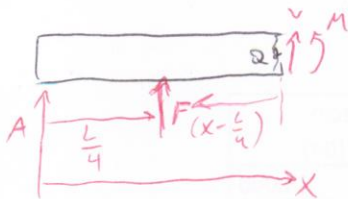
i)  $0 < x < \frac{L}{4}$



$$\sum F_y = 0 \Rightarrow V(x) = A$$

$$\sum M_z = 0 \Rightarrow -Ax + M = 0 \Rightarrow \boxed{M(x) = Ax}$$

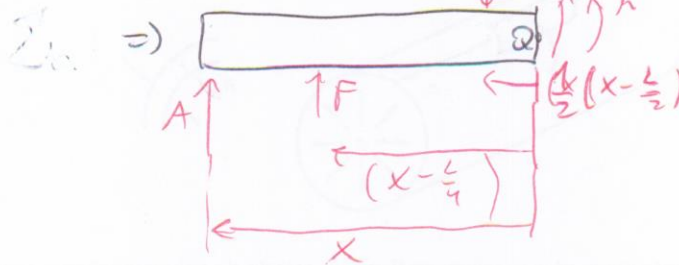
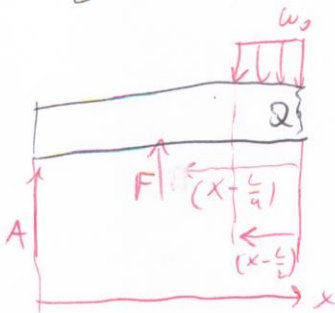
ii)  $\frac{L}{4} < x < \frac{L}{2}$



$$\sum M_z = 0 \Rightarrow -Ax - F(x - \frac{L}{4}) + M = 0$$

$$\boxed{\therefore M(x) = Ax + F(x - \frac{L}{4})}$$

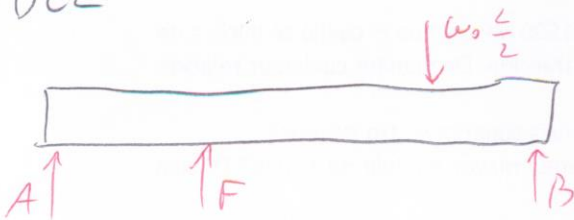
iii)  $\frac{L}{2} < x < L$



$$\sum M_z = 0 \Rightarrow -Ax - F(x - \frac{L}{4}) + \frac{w_0}{2} \left(x - \frac{L}{2}\right)^2 + M = 0$$

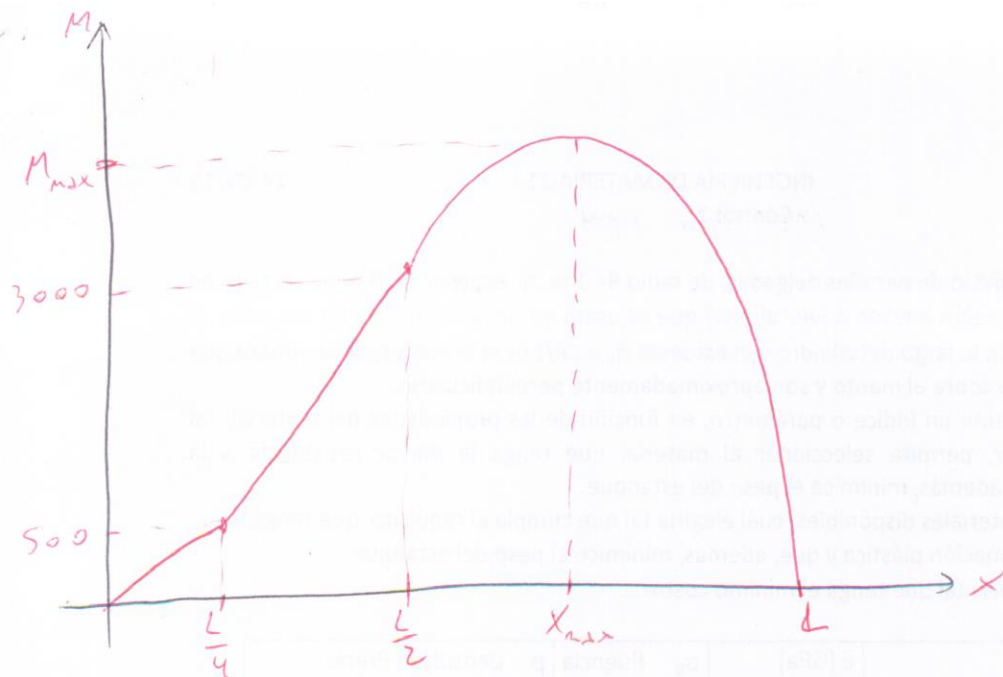
$$\boxed{\therefore M(x) = Ax + F(x - \frac{L}{4}) - \frac{w_0}{2} \left(x - \frac{L}{2}\right)^2}$$

\* DCL



$$\sum M_z = 0 \Rightarrow A \cdot L - F \cdot \frac{3L}{4} + \frac{w_0 L^2}{8} = 0$$

$$\boxed{\therefore A = \frac{w_0 L}{8} - \frac{3}{4} F = 500 \text{ N}}$$



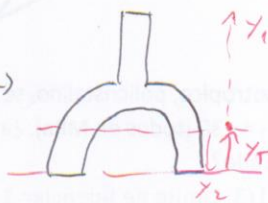
• Si el máximo se encuentra en el 3º tramo:

$$\frac{dM(x)}{dx} \Big|_{M_{max}} = 0 \Rightarrow A + F - w_0 \left( x - \frac{L}{2} \right) = 0$$

$$x_{max} = \frac{A+F}{w_0} + \frac{L}{2} = 2,625 \text{ m}$$

$$\Rightarrow \boxed{M_{max} = 3781,25 \text{ N}\cdot\text{m}}$$

• Es el máximo  $\Rightarrow \sigma = -\frac{M_{max}}{I_z} \cdot y_{max} \rightarrow$



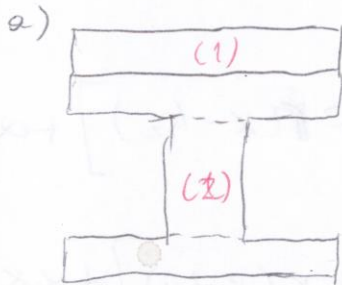
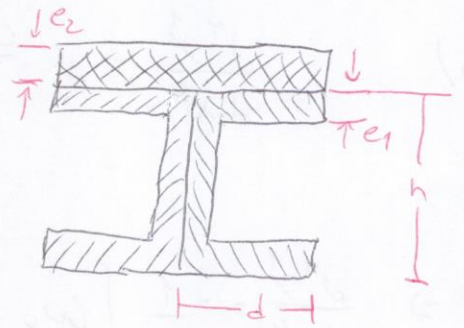
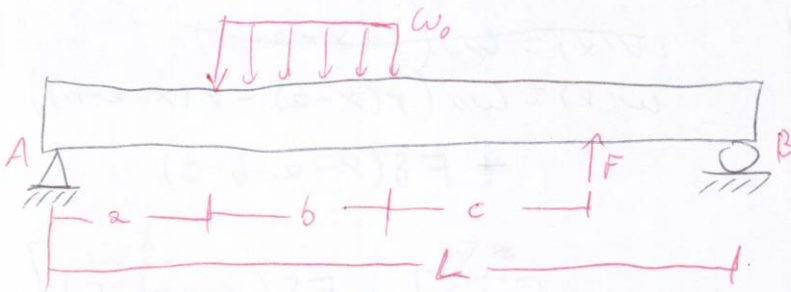
$$y_1 = h - \bar{y}_T$$

$$y_2 = -\bar{y}_T$$

$$\Rightarrow \boxed{y_1 = 9,532 \text{ cm}} \quad \& \quad y_2 = -7,468 \text{ cm}$$

$$\therefore \sigma = \frac{-3781,25 \text{ N}\cdot\text{m}}{4,341 \cdot 10^{-5} \text{ m}^4} \cdot 9,532 \cdot 10^{-2} \text{ m} \Rightarrow \boxed{\sigma_{max} = -8,303 \text{ MPa}}$$

(Compresión)



$$\bar{y}_T = \frac{\sum \bar{y}_i \cdot A_i}{\sum A_i} \quad / \quad \begin{aligned} \bar{y}_1 &= h + \frac{e_2}{2}; A_1 = 2de_2 \\ \bar{y}_2 &= \frac{h}{2}; A_2 = 4de_1 + 2e_1(h-2e_1) \\ &\quad + 2e_1(h-2e_1) \end{aligned}$$

$$\Rightarrow \bar{y}_T = \frac{(h + \frac{e_2}{2}) \cdot 2de_2 + \frac{h}{2} (4de_1 + 2e_1(h-2e_1))}{2de_2 + 4de_1 + 2e_1(h-2e_1)}$$

$$\boxed{\bar{y}_T = 0,177 \text{ m}}$$

$$\sim \bar{I}_2 = \bar{I}_1 + \bar{I}_2$$

$$\hookrightarrow \bar{I}_1 = I_1 + (\bar{y}_1 - \bar{y}_T)^2 \cdot A_1 = \frac{2de_2^3}{12} + (\bar{y}_1 - \bar{y}_T)^2 \cdot 2de_2$$

$$\boxed{\bar{I}_1 = 5,538 \cdot 10^{-5} \text{ [m}^4\text{]}}$$

~~$$\hookrightarrow \bar{I}_2 = \frac{2de_1^3}{12} +$$~~

$$\begin{aligned} * \bar{I}_2 &= \left( \frac{2de_1^3}{12} + \left( \frac{e_1}{2} - \frac{h}{2} \right)^2 \cdot 2de_1 \right) + \left( \frac{2de_1^3}{12} + \left( \frac{h+e_1}{2} - \frac{h}{2} \right)^2 \cdot 2de_1 \right) \\ &\quad + (\bar{y}_T - \bar{y}_2)^2 \cdot A_2 \end{aligned}$$

$$\circ * \bar{I}_2 = 2 \left( \frac{dh^3}{12} - \frac{(d-e_1)(h-2e_1)^3}{12} + (\bar{y}_T - \bar{y}_2)^2 \frac{A_2}{2} \right) = 1,701 \cdot 10^{-4} \text{ m}^4$$



$$* D_c(1) \rightarrow \alpha = \frac{1}{LEI_z} \left[ \omega_0 \left( \frac{(L-a)^2}{2} - \frac{(L-k_1)^2}{2} \right) - F \frac{(L-k_2)^3}{6} \right]$$

$$\alpha = \cancel{3,167 \cdot 10^{-4}} = -7,849 \cdot 10^{-5}$$

\*  $D_c(2)$

$$\gamma = \frac{1}{LEI_z} \left[ \omega_0 \left( \frac{(L-a)^4}{24} - \frac{(L-k_1)^4}{24} \right) - \frac{F(L-k_2)^5}{6} \right] - \frac{\alpha L^2}{6}$$

$$\gamma = 1,402 \cdot 10^{-3}$$

\* Una vez calculadas las ctes., calculamos la deflexión en  $x = L/2$

$$\hat{y}(L/2) = -\frac{1}{EI_z} \left[ \omega_0 \cdot \frac{(L/2 - a)^4}{24} \right] + \frac{\alpha (L/2)^3}{6} + \gamma \cdot \frac{L}{2}$$

$$\hat{y}(L/2) = 5,363 \cdot 10^{-3} \text{ [m]}$$

\* El est. normal máximo se calcula como:

$$\sigma_{\max} = -\frac{M(x)}{I_z}$$

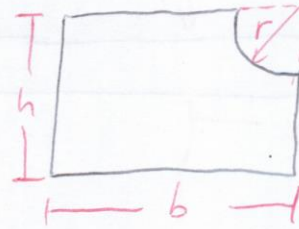
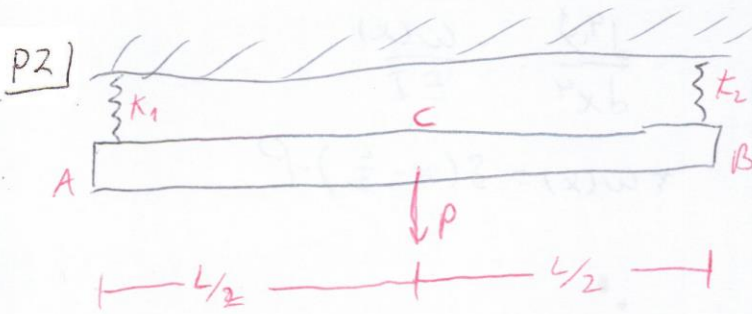
$$\sigma(x) = -\frac{M(x) \cdot \gamma}{I_z} \quad ; \quad M(x) = EI \frac{d^2 \hat{y}}{dx^2}$$

$$\therefore \sigma(x) = -\frac{d^2 \hat{y}}{dx^2} E \gamma$$

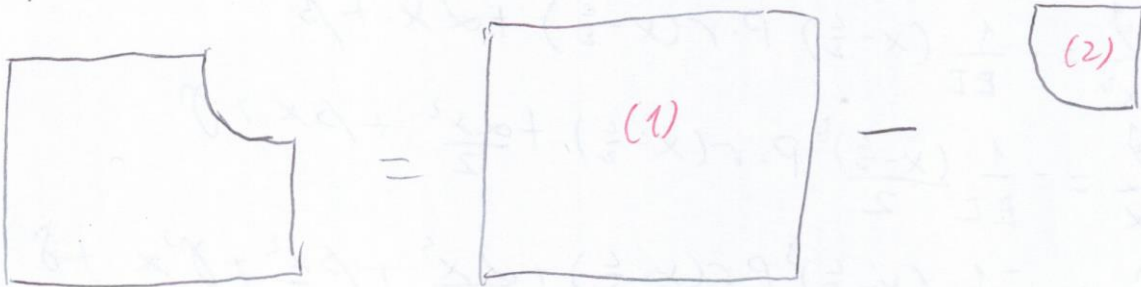
$$\hookrightarrow \frac{d^2 \hat{y}}{dx^2} \left( \frac{L}{2} \right) = -\frac{\omega_0}{2EI_z} \left( \frac{L}{2} - a \right)^2 + \alpha \cdot \frac{L}{2} = -4,279 \cdot 10^{-4}$$

$$\hookrightarrow \gamma_{\max} = -\hat{\gamma}_T = -0,177$$

$$\therefore \sigma(L/2) = \cancel{-28147466} \text{ [Pa]} \quad 1,515 \cdot 10^7 \text{ [Pa]}$$



e) Propriedades de área:



$$(1): \bar{y}_1 = \frac{h}{2} \quad \text{e} \quad I_1 = \frac{b \cdot h^3}{12}$$

$$(2): \left. \begin{array}{l} \bar{y}_2 = \frac{4r}{3\pi} \quad \text{e} \quad I_2 = \frac{\pi r^4}{16} \\ \text{Desde a base} \end{array} \right\} \begin{array}{l} \bar{y}_2 = h - \frac{4r}{3\pi} \end{array}$$

$$\Rightarrow \bar{y}_T = \frac{\bar{y}_1 \cdot A_1 - \bar{y}_2 \cdot A_2}{A_1 - A_2} = \frac{\frac{h}{2} \cdot hb - \left(h - \frac{4r}{3\pi}\right) \cdot \frac{1}{4} \pi r^2}{hb - \frac{1}{4} \pi r^2} = 4,567 \text{ cm}$$

$$\boxed{\bar{y}_T = 4,567 \text{ cm}}$$

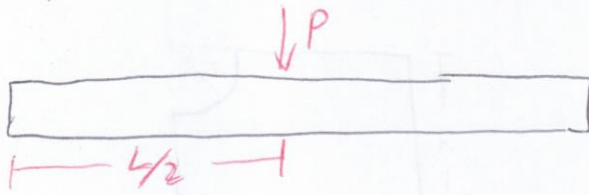
$$\Rightarrow \bar{I}_1 = I_1 + S^2 A = \frac{bh^3}{12} + \left(\frac{h}{2} - \bar{y}_T\right)^2 bh \Rightarrow \boxed{\bar{I}_1 = 1,278 \cdot 10^{-5} \text{ m}^4}$$

$$\bar{I}_2 = I_2 + S^2 A = \frac{\pi r^4}{16} + \left(\bar{y}_T - \left(h + \frac{4r}{3\pi}\right)\right)^2 \cdot \frac{1}{4} \pi r^2 \Rightarrow \boxed{\bar{I}_2 = 3,38 \cdot 10^{-6} \text{ m}^4}$$

$$\therefore \bar{I}_T = \bar{I}_1 - \bar{I}_2 \Rightarrow \boxed{\bar{I}_T = 9,401 \cdot 10^{-6} \text{ m}^4}$$



b) Aplicando la ec. de la curva elástica



$$\frac{d^4 y}{dx^4} = -\frac{w(x)}{EI}$$

$$* w(x) = \delta(x - \frac{L}{2}) \cdot P$$

• Integrando:

$$\rightarrow \frac{d^3 y}{dx^3} = -\frac{1}{EI} \cdot P \cdot r(x - \frac{L}{2}) + \alpha$$

$$\rightarrow \frac{d^2 y}{dx^2} = -\frac{1}{EI} (x - \frac{L}{2}) \cdot P \cdot r(x - \frac{L}{2}) + \alpha x + \beta$$

$$\rightarrow \frac{d y}{dx} = -\frac{1}{EI} \frac{(x - \frac{L}{2})^2}{2} P \cdot r(x - \frac{L}{2}) + \frac{\alpha x^2}{2} + \beta x + \gamma$$

$$\Rightarrow \hat{y}(x) = \frac{-1}{6EI} (x - \frac{L}{2})^3 P r(x - \frac{L}{2}) + \frac{\alpha x^3}{6} + \beta \frac{x^2}{2} + \gamma x + \delta$$

• Condiciones de Borde:

$$\hookrightarrow \left[ \frac{d^2 y}{dx^2}(0) = 0 \text{ (1)} \mid \frac{d^2 y}{dx^2}(L) = 0 \text{ (2)} \right]$$

↳ Corte dif. en  $x=0 \rightsquigarrow$   $\left. \begin{array}{l} \uparrow A \\ \uparrow V \end{array} \right\} \begin{array}{l} V(0) + A = 0 \\ \Rightarrow V(0) = -A \end{array}$

$$* V(x) = -EI \frac{d^3 y}{dx^3}(x) \quad \Rightarrow \quad A = -k_1 \hat{y}'(0)$$

$$\therefore -EI \frac{d^3 y}{dx^3}(0) = k_1 \hat{y}'(0) \text{ (3)}$$

↳ Corte dif. en  $x=L$

$\left. \begin{array}{l} \uparrow B \\ \uparrow V \end{array} \right\} \begin{array}{l} V(L) - B = 0 \Rightarrow V(L) = B \\ * B = -k_2 \hat{y}'(L) \end{array}$

$$\therefore EI \frac{d^3 y}{dx^3}(L) = k_2 \hat{y}'(L) \text{ (4)}$$

• Aplicando las cond. de Borde

$$(1) \frac{d^2 y}{dx^2}(0) = 0 \Rightarrow \boxed{\beta = 0}$$

$$(2) \frac{d^2 y}{dx^2}(L) = 0 \rightsquigarrow -\frac{1}{EI} \left(L - \frac{L}{2}\right) \cdot P + 2L = 0$$
$$\Rightarrow \boxed{\alpha = \frac{P}{2EI}}$$

$$(3) -EI \frac{d^3 y}{dx^3}(0) = K_1 y'(0)$$

$$-2EI = K_1 \delta \rightsquigarrow \delta = -\frac{2EI}{K_1} = -\frac{P}{2EI} \frac{EI}{K_1} \Rightarrow \boxed{\delta = -\frac{P}{2K_1}}$$

$$(4) EI \frac{d^3 y}{dx^3}(L) = K_2 y'(L)$$

$$-P + 2EI = K_2 \left( -\frac{1}{6EI} \left(L - \frac{L}{2}\right)^3 P + \frac{2L^3}{6} + \gamma L + \delta \right)$$

~~\* Despejando~~

$$-P + \frac{P}{2} = K_2 \left( -\frac{L^3 P}{48EI} + \frac{2L^3}{6} + \frac{PL}{2EI} \right) + K_2 L \gamma$$

$$\therefore \gamma = \frac{1}{K_2 L} \left( -\frac{P}{2} + K_2 P \left( -\frac{L^3}{48EI} + \frac{L^3}{12EI} - \frac{1}{2K_1} \right) \right)$$

• Una vez calculadas todas las constantes, evaluamos  $y'(\frac{L}{2})$  para encontrar el desplazamiento en el punto C.

$$y'(\frac{L}{2}) = \alpha \frac{L^3}{6} + \gamma L + \delta = \alpha \frac{\left(\frac{L}{2}\right)^3}{6} + \gamma \frac{L}{2} + \delta$$

• Calculando los coef:  $\alpha = 1,4 \cdot 10^{-3}$   
 $\gamma = -7,4 \cdot 10^{-5}$   
 $\delta = -8,3 \cdot 10^{-3}$

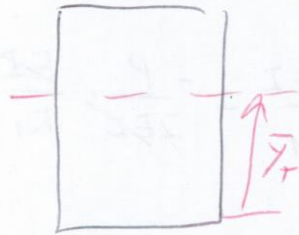
$$\therefore y'(\frac{L}{2}) = -0,0241 \text{ m} = -2,41 \text{ cm}$$

a)  $M = EI \frac{d^2 y}{dx^2} \Rightarrow M_{max} \rightarrow$  derivamos  $M(x)$ , obtenemos  $x$  para luego evaluar en  $M(x)$

$$\Rightarrow \frac{d^3 y}{dx^3} = 0 \Rightarrow \frac{1}{EI} P \cdot r \left(x - \frac{L}{2}\right) + \frac{P}{2EI}$$

c)  $M_{max} \rightarrow \left(\frac{d^2 y}{dx^2}\right)_{max} \rightarrow x = \frac{L}{2}$

$x_{max} \rightarrow$



$$* y = -\bar{y}_+ = -4,967 \text{ cm}$$

$$* y = h - \bar{y}_+ = 5,433 \text{ cm} \rightarrow M_{max} \text{ (Ext. sup)}$$

$$\therefore \sigma_{max} = -\frac{M}{I} \quad \wedge \quad M = EI \frac{d^2 y}{dx^2}$$

$$\Rightarrow \sigma_{max} = -E \gamma_{max} \left(\frac{d^2 y}{dx^2}\right)_{max} \quad \left. \vphantom{\sigma_{max}} \right\} \frac{d^2 y}{dx^2} \left(\frac{L}{2}\right) = \frac{PL}{4EI}$$

$$\boxed{\therefore \sigma_{max} = -43,342 \text{ MPa}}$$